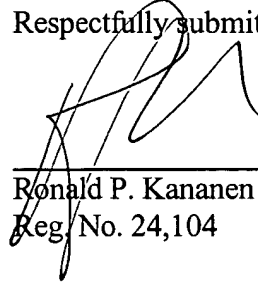


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the undersigned at the number listed below.

Respectfully submitted,

Dated: January 24, 2002



Ronald P. Kananen
Reg. No. 24,104

Rader, Fishman & Grauer PLLC
Suite 501
1233 20TH Street, N.W.
Washington, D.C. 20036
Telephone: (202) 955-3750
Customer No. 23353

Enclosure: Appendix I (Marked-Up Version of Amended Specification)
DC080576

APPENDIX I

MARKED-UP VERSION OF AMENDED SPECIFICATION

On Page 31, Paragraph 3:

If the multiplication factor converting directions of the anamorphic prism are such that $\beta_1 = \beta_A \times \beta_2$, as described above, the shift of the focussing position with respect to the defocussing Δ_{Def} is such that

$$\text{direction 1: } \Delta_1 \approx \Delta_{Def} \times 2 \times (\beta_A \times \beta_2)^2$$

$$\text{direction 2: } \Delta_2 \approx \Delta_{Def} \times 2 \times \beta_2^2$$

On Page 31, Paragraph 4:

The spot diameter ϕ_1 on focussing is given by

$$(S_{pp}/2) \times 2 \times ((\beta_A \times \beta_2)^2 \times \{(2 \cdot NA)/(\beta_A \times \beta_2)\})$$

$$= 2 \cdot NA \cdot S_{pp} \cdot (\beta_A \times \beta_2)$$

...(1).

On Page 32, Paragraph 1:

If, in the above equation 1, the focussing pull-in range S_p is fixed and the spot diameter ϕ_1 on focussing is fixed, the spot diameter ϕ_1 is given by

$$\phi \approx 2 \cdot NA \cdot S_{pp} \cdot (\beta_A \times \beta_2) = \text{constant}$$

so that the multiplication factor β_2 for the direction 2 for detecting the tracking error and the land-groove discrimination signal is in proportion to $1/\beta_A$.

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$$\frac{1}{\beta_A} \cdot \beta_2 \propto \frac{1}{\beta_A}$$

So, the variation of the spot diameter ϕ_2 for the defocussing Δ_{def} is

$$\Delta\phi_2/\Delta Def \approx 4 \cdot NA \cdot \beta_2 \propto 1/\beta_A$$

...(3)

so that it is inversely proportional to the multiplication factor β_A of the anamorphic prism. Meanwhile, if the direction of the multiplication factor of the anamorphic prism is the radial direction, it suffices to substitute $1/\beta_A$ for β_A .